

(a) Component heating \Rightarrow decide cooling ^(size) requirement and possible operating power level

(b) Steadystate VI characteristics [check slide notes]

I_{thyristor} \Rightarrow a threshold voltage needed for conduction, reverse recovery

MOSFET \Rightarrow No threshold voltage, no reverse recovery

operation \Rightarrow thyristor - semi controlled, high power

MOSFET - fully controlled, low power

(c) Calculate I_{sat} [check slide notes]

$N_{sat} = B_{sat} A_c (R_g + R_c)$: Reluctance of core (R_c) & airgap (R_g)
 inductance (L)

\Rightarrow without air gap $i_{sat}' = \frac{B_{sat} A_c \cdot R_c}{N}$, $\left[\begin{matrix} L'' = N^2 / (R_c + l_g) \\ L' = N^2 / R_c \end{matrix} \right]$

with air gap $i_{sat}'' = \frac{B_{sat} A_c \cdot (R_c + R_g)}{N} > i_{sat}'$

operating range for energy stored in the conductor

Energy' = $\frac{1}{2} L' i_{sat}'^2 = \frac{1}{2} B_{sat} A_c N \cdot I_{sat}' < \frac{1}{2} B_{sat} A_c N \cdot i_{sat}'' = \frac{1}{2} L'' i_{sat}''^2$

$N_1 : N_2 : N_3 = 0.5 : 1 : 1$ Flyback Converter

$V_d = 25 \text{ V}$

$f_{sw} = 30 \text{ kHz} \Rightarrow T_s = 1/f_{sw}$

$D = 0.4$

$L_m = 120 \mu\text{H}$

(a) $R_{load} = 15/150 \Omega$, $V_o = ?$ with N_2 , $V_{o,max} = \frac{N_3}{N_2} V_d = \underline{V_d}$

Identify operation Mode CCM/DCM.

For CCM:

$V_o = \frac{N_3}{N_1} \cdot \frac{D}{1-D} V_d = \frac{1}{0.5} \cdot \frac{0.4}{1-0.4} \cdot V_d = \frac{4}{3} V_d > V_d$ (N_2 winding working)

\Rightarrow if CCM, $V_o = V_d$ (2)

During S on, $L_m \frac{\Delta i_m}{DT_s} = V_i = V_d$

$\Rightarrow \Delta i_m = \underline{4.17 \text{ A}}$

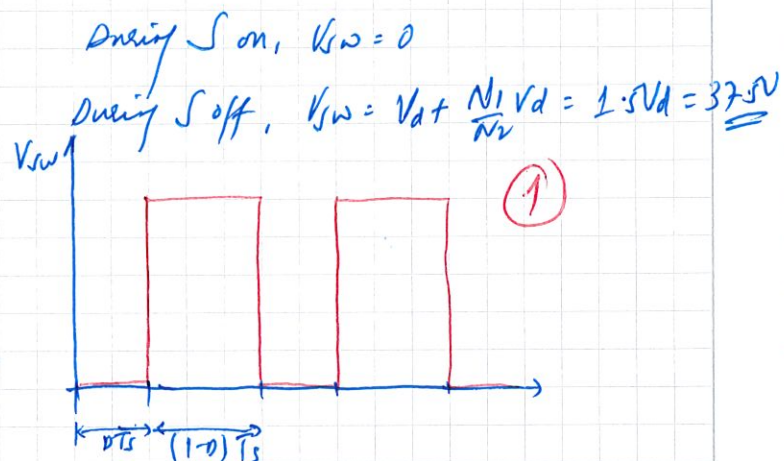
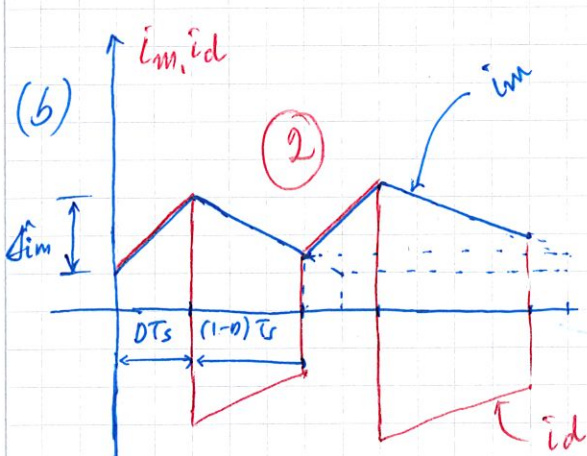
During S off, D_2 conducts $\Rightarrow -\frac{L_m \Delta i_m}{D_1 T_s} = V_2 \cdot \frac{N_1}{N_2} = 0.5 V_d$

for $\Delta i_m = 4.17 \Rightarrow$ the demagnetizing time $D_1 = 2D = 0.8$

but $D + D_1 = 1.2 > 1 \Rightarrow$ the magnetizing current keeps increasing

As there is no enough demagnetizing time, the converter works in CCM mode all the time for $R_{load} = 15\Omega / 150\Omega$. (2)

$\Rightarrow V_o = V_d = 25 \text{ V}$, $\Rightarrow i_D = 0$



Forward Converter

$N_1 : N_3 : N_2 = 2 : 1 : 2$

$V_o = 20\text{V}$

$P_o = 60\text{W}$

$V_d = 30\text{V}$

$f_{sw} = 30\text{kHz}$, $\Rightarrow T_s = 1/f_{sw}$

(a) $\Delta i_L = 0.15 I_L$, $\Delta i_m = 0.015 I_L$ ($I_L = I_o$)

$I_L = I_o = P_o / V_o = 3\text{A}$

$\Rightarrow \Delta i_L = 0.45\text{A} \Rightarrow$ During Sw on, $v_L = \frac{L \Delta i_L}{DT_s} = \frac{N_2}{N_1} V_d - V_o \Rightarrow 0.45$

$\Delta i_m = 0.045\text{A} \Rightarrow$ During Sw on, $v_1 = V_d = L_m \frac{\Delta i_m}{DT_s} \Rightarrow 0.045$

} $D = ?$

$\Delta i_L \neq 4 I_L \Rightarrow \frac{\Delta i_L}{2} = 0.225\text{A} < I_L = I_o = 3\text{A} \Rightarrow \text{CCM}$

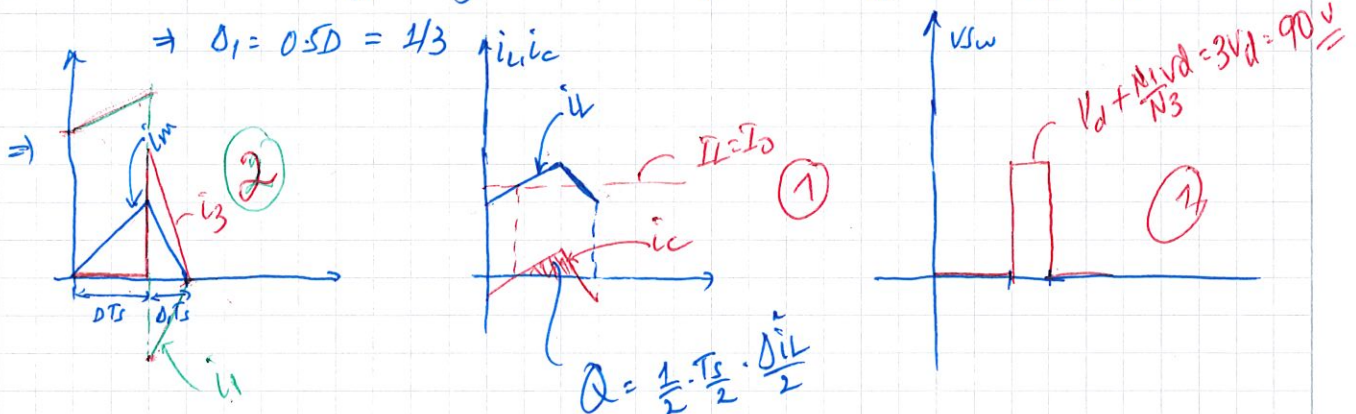
$\Rightarrow V_o = \frac{N_2}{N_1} \cdot D V_d \Rightarrow D = N_1 / N_2 \cdot V_o / V_d = \frac{V_o}{V_d} = \underline{0.67} \approx 2/3$ (1)

$\therefore L = \frac{DT_s (V_d - V_o)}{\Delta i_L} \text{ H} = \underline{0.496\text{mH}}$ (1)

$L_m = \frac{DT_s (V_d)}{\Delta i_m} \text{ H} = \underline{14.9\text{mH}}$ (1)

(b) refer the slide notes for waveforms.

For Δi_m , $\Delta t_1 =$ demagnetizing time = ? For Sw off, $V_1 = \frac{N_1}{N_3} V_3 = \frac{N_1}{N_2} V_d = -2V_d$



$$(c) \Delta V_o = 0.02 V_o = 0.4V = \frac{1/2 (\Delta i_{in}/2) (T_s/2)}{C_{min}} = Q_{area}/C_{min}$$

$$\Rightarrow C_{min} = \frac{1/8 (\Delta i_{in}) (1/f_{sw})}{\Delta V_o} = \frac{1/8 (0.45) (1/30 \times 10^3)}{0.4} F = \underline{\underline{4.69 \mu F}} \quad (2)$$

$$(d) f_c = \frac{1}{2\pi} \sqrt{\frac{1}{LC}} \text{ Hz} = \frac{1}{2\pi} \sqrt{\frac{1}{0.496(10^{-3})(4.69(10^{-6}))}} \text{ Hz} = \underline{\underline{3.3 \text{ kHz}}} \quad (1)$$

$f_c \ll f_{sw} = 30 \text{ kHz} \Rightarrow$ good filtering of harmonics
can be achieved! (1)

(a) ac-current harmonics : 3, 5, 7, 9, 11 --- $2n+1$
 dc-current harmonics : 2, 4, 6, --- $2n$ } 1-phase (2)

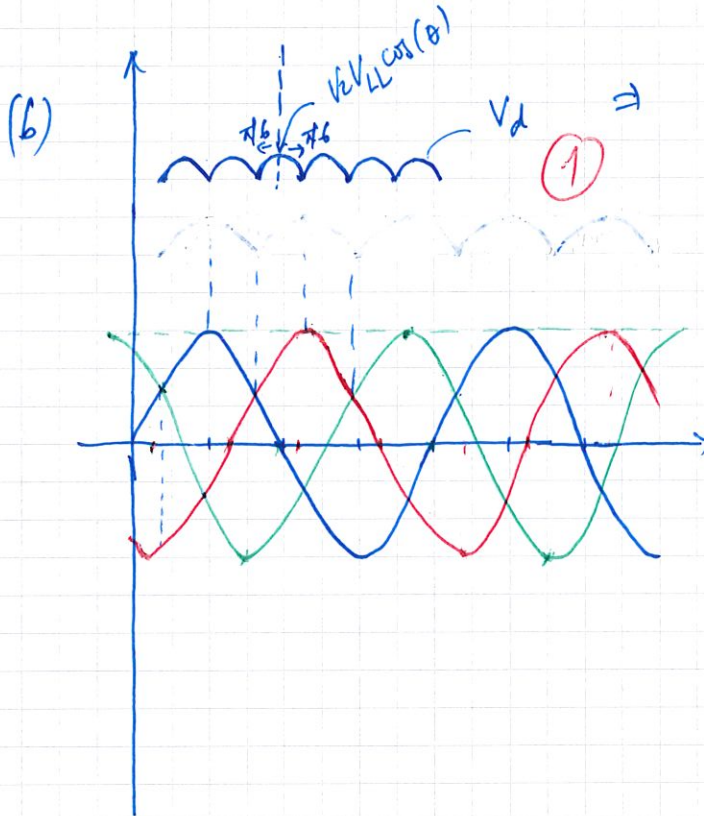
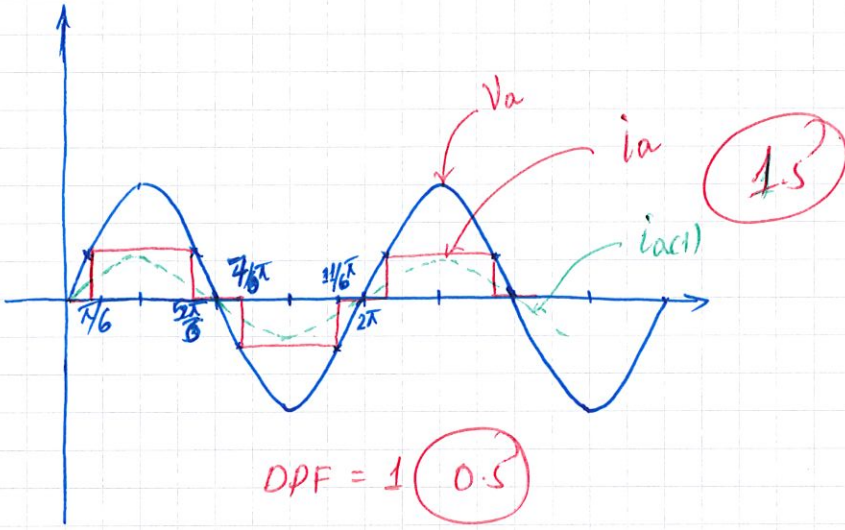
ac-current harmonics : 5, 7, 11, 13 --- $6n+1$
 dc-current harmonics : 6, 12, --- $6n$ } 3-phase (2)

(b) advantage :: higher fundamental output voltage
 :: long modulation (1)
 :: less switching losses

disadvantage :: uncontrolled output voltage
 :: low order harmonics (1)

(c) use PWM modulation with higher frequency of the triangular waveform (2)

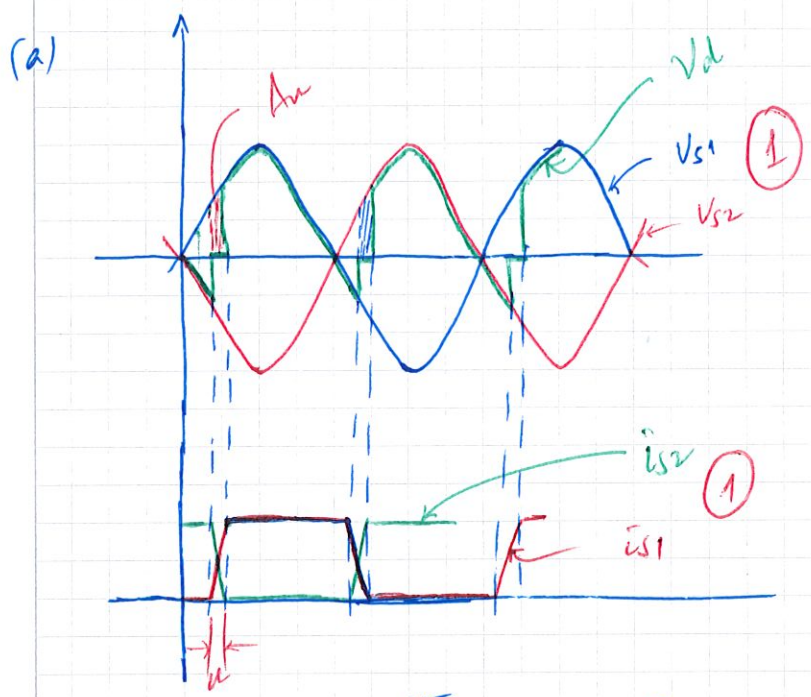
a) $I_d = 15A$, $50Hz$, $V_{LL} = 400V$



$$V_d = \frac{1}{\pi/3} \int_{-\pi/6}^{\pi/6} \sqrt{2} V_{LL} \cos(\theta) d\theta = \frac{1}{\pi/6} \int_0^{\pi/6} \sqrt{2} V_{LL} \cos(\theta) d\theta$$

$$= \frac{3\sqrt{2}}{\pi} V_{LL} \quad r = \underline{\underline{340V}}$$

$L_s = 5 \text{ mH} \quad , \quad f = 50 \text{ Hz}$
 $I_d = 25 \text{ A}$
 $v_{s1} = 180 \sin(\theta)$
 $v_{s2} = 180 \sin(\theta - \pi)$
 $\alpha = 30^\circ = \pi/6 \text{ rad}$



$$V_d = \frac{1}{\pi} \left[\int_{\alpha}^{\alpha+\pi} v_d d\theta - A_u \right] \quad ; \quad v_d = v_{s1} = 180 \sin(\theta)$$

$A_u = ? \quad v_{s1} - v_{s2} - L_s \frac{di_{s1}}{dt} + L_s \frac{di_{s2}}{dt} = 0$ during commutation

$\Rightarrow 2L_s \frac{di_{s1}}{dt} = v_{s1} - v_{s2} \quad \Downarrow \quad i_{s2} = I_d - i_{s1}$

$\Rightarrow L_s \frac{di_{s1}}{dt} = \frac{1}{2} (v_{s1} - v_{s2})$

$A_u = \int_0^{\alpha+\pi} \frac{1}{2} (v_{s1} - v_{s2}) d\theta = \int_0^{I_d} L_s \frac{di_{s1}}{dt} \cdot d\theta = \int_0^{I_d} \omega L_s \frac{di_{s1}}{dt} \cdot dt = \omega L_s I_d$

$\Rightarrow V_d = \frac{1}{\pi} \int_{\alpha}^{\alpha+\pi} 180 \sin(\theta) d\theta - \frac{\omega L_s I_d}{\pi} = \frac{180 [2 \cos(\alpha)]}{\pi} - \omega L_s I_d = 91.7 \text{ V}$

(b) $\alpha = 150^\circ \Rightarrow V_d = \frac{180 [2 \cos(150^\circ)]}{\pi} - \omega L_s I_d = -106.7 \text{ V}$

(c) $\alpha = 0^\circ, L_s = 0 \Rightarrow A_u = 0 \Rightarrow$ plot i_{s1}, i_{s2} with $\alpha = 0, u_{s1} = 0 \neq v_d$. $V_d = 180 [2] / \pi = 114.6 \text{ V}$

$$P = 2.5 \text{ W}$$

$$T_a = 20^\circ \text{C}$$

$$R_{thja} = 62^\circ \text{C/W}$$

$$(a) \quad T_j = T_a + P[R_{thja}] = 20^\circ + 2.5(62) = \underline{175^\circ \text{C}} > T_{jmax}$$

heat sink needed

(2)

$$(b) \quad T_{jmax} = 100 = T_a + P[R_{thja}] = 20^\circ + 2.5[R_{thja}]$$

$$\Rightarrow R_{thja} = \frac{100^\circ - 20^\circ}{2.5 \text{ W}} = \underline{\underline{32^\circ \text{C/W}}}$$

(2)